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## DESCRIPTION

INKJET PRINT DEVICE,  
INKJET PRINT METHOD FOR THE DEVICE,  
INKJET PRINT COMPUTER PROGRAM,  
5 AND  
STORAGE MEDIUM CONTAINING THE COMPUTER PROGRAM

## TECHNICAL FIELD

The present invention relates to inkjet printers and like  
inkjet print devices, in particular, those inkjet print devices  
10 which print by reciprocally moving a carriage carrying a print  
head in a main scan direction while controlling ink ejection  
from the print head according to information on the position  
of the carriage both in a forward movement and in a return  
movement.

## BACKGROUND ART

In an inkjet print device of this type, the carriage, in its  
movement in the main scan direction, temporarily halts at  
each end of its mobility range before going on in an opposite  
20 direction. Thus, there is an accelerate/decelerate area at each  
end of the mobility range and a constant-speed area there  
between.

In addition, as the print head ejects ink while the

carriage is moving, the ink hits recording paper at a position somewhat ahead of where it was ejected with respect to the direction of the movement. Therefore, if ink is ejected when the carriage is at the same position in the forward and return directions, aiming at the same position on an image with respect to the main scan direction, the ink hits different positions. To avoid such off-target hitting, the ink eject position needs be corrected at least either in the forward movement or in the return movement to hit the same position on the image.

The magnitude of the discrepancy between the ink eject position and the ink hitting position varies with the moving speed of the carriage (hereinafter, "carriage speed"). The ink eject position can be corrected relatively easily in the constant-speed area, but difficult in the accelerate/decelerate areas. In conventional inkjet print devices, therefore, print areas are specified inside the constant-speed area so that the print device prints only inside the constant-speed area.

Problems arise with the specification of print areas only inside the constant-speed area in the conventional inkjet print device. Printing takes time because of the presence of the accelerate/decelerate areas extending from the ends of the constant-speed area. For the same reason, the device is bulky too.

Further, the inkjet print device senses the carriage

position with a linear encoder. Commercially available  
encoder have a maximum resolution of 150 dpi, whilst the  
image printed on recording paper has a resolution of 600 to  
1200 dpi. The encoder output cannot be used straightly as  
5 position information to control ink ejection in high resolution  
printing.

#### DISCLOSURE OF INVENTION

The present invention, conceived to address these  
10 problems, has an objective to provide an inkjet print device  
capable of high resolution printing in the  
accelerate/decelerate areas that flank the constant-speed  
area for reduced print time and reduced device size.

To achieve the objective, an inkjet print device in  
15 accordance with the present invention is an inkjet print  
device which prints by reciprocally moving a carriage carrying  
a print head in a main scan direction while controlling ink  
ejection from the print head according to a carriage position  
both in a forward movement and in a return movement, and is  
20 characterized in that the device contains: position sensing  
means for sensing the carriage position; speed sensing means  
for sensing moving speed of the carriage; correction quantity  
determining means for presetting a relationship between the  
speed of the carriage and a positional correction quantity for  
25 correcting a discrepancy in an ink hitting position resulting

from the ink ejection from the print head while the carriage is moving and for determining the positional correction quantity from the carriage speed sensed by the speed sensing means according to the preset relationship; and ejection control means for controlling the ink ejection from the print head according to the positional correction quantity determined by the correction quantity determining means and the carriage position sensed by the position sensing means.

According to the arrangement, even if the carriage speed changes, a suitable positional correction quantity is obtainable according to the relationship between the positional correction quantity and the carriage speed. Thus, the ink ejection from the print head is controlled based on a suitable positional correction quantity. Good image quality is available even while the carriage is accelerating or decelerating. Hence, the device can print in the accelerate/decelerate areas flanking the constant-speed area, achieving reduced print time and reduced device size.

For a fuller understanding of the nature and advantages of the invention, reference should be made to the ensuing detailed description taken in conjunction with the accompanying drawings.

#### BRIEF DESCRIPTION OF DRAWINGS

Figure 1 is a partially exploded side view showing major

features of an inkjet printer which is an embodiment of the present invention.

Figure 2 is a front view showing part of the structure inside the inkjet printer.

5        Figure 3 is a block diagram showing, as an example, the electrical arrangement of a major part of the inkjet printer.

Figures 4(a), 4(b) are illustrations showing how a carriage speed changes with print areas. Figure 4(a) is related to the inkjet printer of the present embodiment, and Figure  
10       4(b) to the conventional inkjet printer.

Figures 5 are drawings illustrating a discrepancy between the ink eject position and the ink hitting position.

Figure 6 is a drawing illustrating discrepancies in the positions of those dots formed in a forward movement and  
15       those dots formed in a return movement.

Figure 7 is a drawing illustrating matching of the dots formed in the forward movement and the dots formed in the return movement after correction in the forward movement and in the return movement.

20       Figure 8 is a drawing illustrating matching of the dots formed in the forward movement and the dots formed in the return movement after correction in the return movement only.

Figure 9 is a functional block diagram showing, as an  
25       example, the functions and arrangement of a control section

related to ink ejection control.

Figure 10 is time charts showing exemplary encoder output signals.

5 Figure 11 is a flow chart showing, as an example, a process by a first U/D counter.

Figure 12 is a flow chart showing, as an example, an interrupt process by the first U/D counter on a timer.

10 Figure 13 is a flow chart showing, as an example, an interrupt process by an interval timer on a second U/D counter.

Figure 14 is a flow chart showing, as an example, a corrected position computing process and an ink ejection control process.

15 Figure 15 is a flow chart showing, as an example, changes in the ink ejection control process in Figure 14.

Figure 16 is a functional block diagram showing, as another example, the functions and arrangement of a control section related to ink ejection control.

20 Figure 17 is a flow chart showing, as an example, a process by a U/D counter.

#### BEST MODE FOR CARRYING OUT THE INVENTION

25 Referring to figures, the following will describe an embodiment in which the present invention is applied to an inkjet printer.

Figure 1 is a schematic showing the overall structure of an inkjet printer. In the following, directional descriptions will be given with respect to a transport direction of recording paper (detailed later). The front refers to the downstream direction, and the back to the upstream. The left/right are defined as looking at the front. Thus, in Figure 1, the left-hand side is the front, the right-hand side is the back, the front of the paper is the left, and the back of the paper is the right. Figure 2 illustrates a part of the internal structure of the inkjet printer in Figure 1 as viewed from the front.

In the following, ordinary numerals represent decimal numbers, while bracketed numerals and letters, A to F, represent hexadecimal numbers. An A, B, C, D, E, and F in hexadecimal notation are equal to a decimal 10, 11, 12, 13, 14, 15, and 16 respectively.

Referring to Figure 1, the device main body of the printer is a box housing (1). There are provided a paper feed tray (2) in the far back of the housing (1) and a paper discharge tray (3) in the near front of the housing (1). Between the paper feed tray (2) and the paper discharge tray (3) in the housing (1) are provided a paper feed section (4), a transport section (5), a print section (6), and a paper discharge section (7).

The paper feed tray (2) contains one or more pieces of recording paper (P) with the print surface looking forward,

but slightly upward. The paper feed section (4) supplies recording paper (P) a piece at a time from the paper feed tray (2) to the transport section (5). The paper feed section (4) includes a separator device (8) and a paper feed roller (9). The separator device (8) is positioned slightly toward the front from, and lower than, the bottom end of the recording paper (P) on the paper feed tray (2). The paper feed roller (9) presses down the separator device (8). The paper feed tray (2) has a press device (10) which moves the recording paper (P) toward the paper feed roller (9) to feed the paper to the roller (9).

The transport section (5) transports recording paper (P) fed from the paper feed section (4) to the print section (6). The transport section (5) includes a guide board (11) toward the front from the separator device (8) and a pair of top and bottom supply rollers (12), (13) further toward the front.

The print section (6) prints on recording paper (P) coming from the transport section (5). The print section (6) includes a platen (14) toward the front from the pair of supply rollers (12), (13) and a carriage (15) above the platen (14).

Now referring to Figure 2, the print section (6) includes a guide bar (16) extending in the left/right directions which matches the main scan directions. The carriage (15) sits on the guide bar (16) so that it is movable. A print head (17) is mounted on the bottom of the carriage (16). Although not shown in the figure, a set of ink nozzles is formed on the



bottom of the print head (17). The carriage (15) is mounted to a timing belt (18) driven by an electromotor (DC motor) which is omitted from Figure 1. Thus, the carriage (15) is reciprocally moved in the left/right directions along the guide bar (16).

The paper discharge section (7) discharges recording paper (P) printed by the print section (6) from the paper discharge tray (3). The paper discharge section (7) includes a paper discharge roller (19) toward the front, and lower than, the platen (14) and a spur (20) pressing down the paper discharge roller (19).

For the printer to print, first, the press device (10) acts to press, again the paper feed roller (9), the bottom end (front end) of a piece of recording paper (P) which is closest to the front on the paper feed tray (2). Thanks to the rotation of the paper feed roller (9) and the action of the separator device (8), that sheet alone is moved on the guide board (11) and fed between the supply rollers (12), (13). The supply rollers (12), (13) rotate in concert with the action of the print section (6). After transporting recording paper (P) to a predetermined print start site for the print section (6), the supply rollers (12), (13) transport moves the recording paper (P) toward the front by a predetermined pitch at a time. Meanwhile, the carriage (15) is reciprocally moved in the left/right directions so that the print section (6) prints on a surface (top face) of the

recording paper (P). The front part of the recording paper (P) where printing is over is moved toward the front by the paper discharge roller (19) and the spur (20). After the completion of the printing, the recording paper (P) is discharged passing  
5 between the paper discharge roller (19) and the spur (20) onto the paper discharge tray (3).

In this printer, the carriage (15) is reciprocally moved in the left/right directions, and ink ejection from the print head (17) is controlled according to information on the position of  
10 the carriage (15) while the carriage is moving in a forward direction and in a return direction to accomplish printing.

Here, the left/right directions (main scan direction) which are the scan direction for the carriage (15) are designated as an x direction. The forward/backward  
15 directions (auxiliary scan direction) which are the transport direction for the paper (P) is designated as a y direction. In addition, a movement of the carriage (15) in the increasing direction on the x axis is defined as a forward movement, and a movement of the carriage (15) in the decreasing direction on  
20 the x axis is defined as a return movement.

Figure 3 illustrates an exemplary electrical arrangement of parts of the print section (6) associated with the transport of the paper (P), motion of the carriage (15), and control of ink ejection from the print head (17). In the figure, an X  
25 motor (21) is the aforementioned electromotor moving the

carriage (15) in the left/right directions. A linear encoder (22) senses the position of the carriage (15) in the left/right directions. A Y motor (23) is an electromotor (pulse motor) driving the supply roller (13) and the paper discharge roller (19) to transport the paper (P).

The printer includes a control section (24) controlling the whole printer. The control section (24) may be a CPU or other compute means executing computer programs loaded into a ROM, RAM, or other storage means.

The control section (24) includes, among others, a drive system control section (25) controlling a drive system including the X motor (21), the Y motor (23), etc., a head control section (26) controlling the print head (17), and an image processing section (27) processing image data and transmitting it to the head control section (26) for a printout.

Figures 4(a), 4(b) show changes in the speed of the carriage (15) in its movement in the left/right directions. They also show a relationship between a mobility range of the carriage (15) and a print area. Figure 4(a) relates to the printer in accordance with the present embodiment. Figure 4(b) relates to a conventional printer.

As shown in Figures 4(a), 4(b), there are accelerate/decelerate areas at the left/right ends of the mobility range of the carriage (15) and a constant-speed area there between.

The conventional printer (see Figure 4(b)) has no print area outside the constant-speed area. In contrast, the printer in accordance with the present embodiment has an expanded print area inclusive of the constant-speed area and the accelerate/decelerate areas flanking that area.

The head control section (26) controls ink ejection from the print head (17) according to information on the position of the carriage (15) in the left/right directions. Further, to correct for the discrepancy in the ink hitting position resulting from the print head (17) ejecting ink while the carriage (15) is moving in the accelerate/decelerate areas, the head control section (26) implement the following procedures. The position and speed of the carriage (15) are sensed. A positional correction quantity at a sensed carriage speed is calculated from a positional correction quantity at a predetermined carriage speed. Ink ejection from the print head (17) is controlled on the basis of the sensed carriage position and the positional correction quantity.

As described, as the print head (17) ejects ink while the carriage (15) is in motion, the ink hits the recording paper (P) at a position forward from the ink eject position with respect to the direction in which the carriage is moving. The magnitude of the discrepancy in the ink hitting position varies with the speed of the carriage (15).

Figures 5 show discrepancy between the ink eject

position and the ink hitting position. Figure 5(a) shows a discrepancy occurring in the forward movement. Figure 5(b) shows a discrepancy in the return movement. Figure 5(c) shows a discrepancy in the forward movement combined with a discrepancy in the return movement. In Figures 5, the right-hand side is the positive direction of the x axis, and the left-hand side is the negative direction of the x axis.

Referring to Figure 5(a) showing the forward movement, an ink hitting position  $X_f$  is more positive on the x axis than an ink eject position  $X_h$ . Referring next to Figure 5(b) showing the return movement, the ink hitting position  $X_r$  is more negative on the x axis than the ink eject position  $X_h$ . If the carriage speed is equal, the magnitude of discrepancy either in the forward movement or in the return movement ("single-direction discrepancy") is equal to that in the other direction. The single-direction discrepancy when the carriage speed is  $V_0$  is indicated by  $dX_0$ .

Assume, for example, that: the carriage speed  $V_0$  is 10 ips (inches per second); the distance,  $L$ , from the print head (17) to the recording paper (P) is 1 mm; the speed,  $V_i$ , at which ink is ejected from the print head (17) is 8 m/s, and the single-direction discrepancy  $dX_0$  is equivalent to 3 dots at 2400 dpi. Now referring to Figure 5(c), ink is ejected at the same ink eject position  $X_h$  in the forward movement and in the return movement. The discrepancy,  $dX_1 (= X_f - X_r)$ , between

the ink hitting position  $X_f$  in the forward movement and the ink hitting position  $X_r$  in the return movement (double-direction discrepancy) is a sum of a discrepancy in the forward movement and a discrepancy in the return movement. Assuming that the carriage speed is  $V_0$  both in the forward movement and the return movement, the double-direction discrepancy  $dX_1$  is twice the single-direction discrepancy  $dX_0$ . Figure 6 shows discrepancies between the dots formed in the forward movement and those formed in the return movement under these conditions.

The ink ejection control is done taking the carriage speed  $V_0$  as a reference and either the single-direction discrepancy  $dX_0$  at the reference speed  $V_0$  as a reference correction quantity (single-direction reference correction quantity) or the double-direction discrepancy  $dX_1$  at the reference speed  $V_0$  as a reference correction quantity (double-direction reference correction quantity).

Figure 7 shows a control based on the single-direction reference correction quantity  $dX_0$ . In this case, the control is done based on the single-direction reference correction quantity  $dX_0$  so that the ink ejected at a dot position  $X_d$  in an image in the return movement can hit the same position on paper (P) as the ink ejected at the same dot position  $X_d$  in the forward movement.

Figure 7 assumes an equal speed of  $V_0$  in the forward

movement and in the return movement. Under these conditions, when the carriage reaches the ink eject position  $X_h$  in the forward movement, ink is ejected aiming at a dot position ( $= X_h + dX_0$ ) on the image which is more positive than the position  $X_h$  by the single-direction reference correction quantity  $dX_0$ . Then, when the carriage reaches the ink eject position  $X_h$  in the return movement, ink is ejected aiming at a dot position ( $= X_h - dX_0$ ) on the image which is more negative than the position  $X_h$  by a single-direction reference correction quantity  $dX_0$ . As a result, as shown in Figure 7, aiming at the same dot position  $X_d$  on the image, ink is ejected when the carriage reaches the ink eject position  $X_h (= X_d - dX_0)$  which is more negative than the dot position  $X_d$  by the single-direction correction quantity  $dX_0$  in the forward movement and when the carriage reaches the ink eject position  $X_h (= X_d + dX_0)$  which is more positive than the dot position  $X_d$  by the single-direction correction quantity  $dX_0$  in the return movement.

The single-direction discrepancy is substantially proportional to the carriage speed. Therefore, if the carriage speed is not equal to the reference speed  $V_0$ , a single-direction correction quantity  $dX(t)$  is calculated as given by equation (1) from the reference speed  $V_0$ , the single-direction reference correction quantity  $dX_0$ , and the sensed carriage speed  $V(t)$ . A similar ink ejection control is possible based on this

single-direction correction quantity  $dX(t)$ .

$$dX(t) = dX0 \times V(t)/V0 \dots (1)$$

The single-direction positional correction quantity is also obtainable from a sensed carriage speed in reference to a correction quantity table prepared in advance. The table contains single-direction positional correction quantities at given carriage speeds. The table can be created through proportionality computation on the single-direction reference correction quantity  $dX0$  at the reference speed  $V0$ .

Figure 8 illustrates control based on the double-direction reference correction quantity  $dX1$ . In this case, the positional correction quantity is made 0 for the control either in the forward movement or in the return movement so that the dot formed in the forward movement and the dot formed in the return movement for identical dot position  $X_d$  hits the paper (P) at the identical positions. In the movement in the other direction, the control is done based on the double-direction reference correction quantity  $dX1$ .

Figure 8 shows when the speed is  $V0$  in the forward movement and the return movement. Under these conditions, in the forward movement, ink is ejected corresponding to an identical dot position on the image (=  $X_h$ ) to the position  $X_h$  at the ink eject position  $X_h$ . In the return movement, ink is ejected corresponding to a dot position on the image (=  $X_h - dX1$ ) which is more negative than the position  $X_h$  by the



double-direction reference correction quantity  $dX1$  at the ink eject position  $Xh$ . As a result, as shown in Figure 8, with respect to the identical dot positions  $Xd$  on the image, ink is ejected at the ink eject position  $Xh (= Xd)$  which is identical to the dot position  $Xd$  in the forward movement and at the ink eject position  $Xh (= Xd + dX1)$  which is more positive than the dot position  $Xd$  by the double-direction correction quantity  $X1$  in the return movement. A control may be done based on the double-direction reference correction quantity  $dX1$  in the forward movement and with a zero positional correction quantity in the return movement.

The double-direction discrepancy is substantially proportional to the carriage speed. Therefore, if the carriage speed is not equal to the reference speed  $V0$ , a double-direction correction quantity  $dX(t)$  is calculated as given by equation (2) from the reference speed  $V0$ , the double-direction reference correction quantity  $dX1$ , and the sensed carriage speed  $V(t)$ . A similar ink ejection control is possible based on this double-direction correction quantity  $dX(t)$ .

$$dX(t) = dX1 \times V(t)/V0 \dots (2)$$

The double-direction positional correction quantity is also obtainable from a sensed carriage speed in reference to a correction quantity table prepared in advance. The table contains double-direction positional correction quantities at

given carriage speeds. The table can be created through proportionality computation on the double-direction reference correction quantity  $dX1$  at the reference speed  $V0$ .

5 The carriage speed is sensed from the output of the encoder (22). The cycle of the pulse signal output of the encoder (22) (hereinafter, "output pulse cycle") is inversely proportional to the carriage speed. Therefore, the single-direction reference correction quantity  $dX0$  or the double-direction reference correction quantity  $dX1$  for the  
10 encoder output pulse cycle (reference pulse cycle)  $T0$  at the reference speed  $V0$  is prepared in advance. Using these and the sensed encoder output pulse cycle  $T(t)$ , the single-direction positional correction quantity  $dX(t)$  or the double-direction positional correction quantity  $dX(t)$  is given  
15 by equation (3).

$$dX(t) = dX0 \times T0/T(t) \dots (3)$$

$$dX(t) = dX1 \times T0/T(t) \dots (4)$$

The single-direction positional correction quantity (or double-direction reference correction quantity) is also  
20 obtainable from an encoder output pulse cycle at the sensed carriage speed in reference to a correction quantity table prepared in advance. The table contains single-direction positional correction quantities (or double-direction positional correction quantities) for the encoder output pulse cycle at  
25 given carriage speeds. The table can be created through

proportionality computation on the single-direction reference correction quantity  $dX0$  (or double-direction reference correction quantity  $dX1$ ) for the reference pulse cycle  $T0$  at the reference speed  $V0$ .

5           Next, referring to Figure 9 to Figure 14, will be described an example of steps of determining a single-direction positional correction quantity from an encoder output pulse cycle and controlling ink ejection based on the single-direction positional correction quantity.

10           Figure 9 shows functions and arrangement of a part of the control section (24) related to the control.

          In Figure 9, an X motor control section (28) is a part of the drive system control section (25) in Figure 3 which controls the X motor (21). The control section (24) includes a  
15           first U/D (up/down) counter (29), a second U/D counter (30), a timer (31), an interval timer (32), a TBL memory (33), and an adder (34).

          The encoder (22) outputs two 150-dpi pulse signals A and B shown in Figure 10 as a result of the movement of the  
20           carriage (15). The two signals A and B are out of phase from each other by a quarter cycle. In a forward movement, the signals A and B changes left to right in Figure 10. In a return movement, the signals A and B changes right to left in Figure 10.

25           The first U/D counter (29) counts the pulses of the

signal A from the encoder (22) to obtain first position information CNT1 which is nothing but the count. The resolution of the first position information CNT1 is 150 dpi. He first position information CNT1 is 12 bits, and its maximum value is equivalent to 693 mm. The first U/D counter (29) determines, from the output signals A, B from the encoder (22), whether the carriage (15) is moving in the forward direction or in the return direction and outputs a signal F/R indicating either the forward movement or the return movement to the second U/D counter (30).

The timer (31) measures time by counting predetermined clock pulses. By calculating a difference between a time-measure count  $T_n$  when the signal A rises and a time-measure count  $T_{n-1}$  when the signal A rose last time, the pulse cycle  $T(t)$  ( $= T_n - T_{n-1}$ ) of the current signal A is determined which is then output to the TBL memory (33). In addition, the count of the pulse cycle  $T(t)$  right-shifted by 4 bits to divided it by 16 for output to the interval timer (32).

The interval timer (32) measures time by counting the same clock pulses as the timer (31). Every time the time-measure count reaches the encoder output pulse cycle  $T(t)$  divided by 16 ( $= T(t)/16$ ), the interval timer (32) outputs a timeout signal TMOUT to the second U/D counter (30).

The second U/D counter (30) counts timeout signals TMOUT from the interval timer (32) to obtain second position

information CNT2 which is nothing but the count. The second position information CNT2 is 4 bits, and the value is from 0 to 15. As would be obvious from the description, the timeout signal TMOUT is output at a cycle of the encoder output pulse cycle  $T(t)$  divided by 16. Therefore, the resolution of the second position information CNT2 is 2400 dpi, or  $1/16$  times the resolution (150 dpi) of the first position information CNT1.

The TBL memory (33) stores the reference encoder output pulse cycle  $T_0$  and the single-direction reference positional correction quantity  $dX_0$  at the reference speed  $V_0$  of the carriage (15). The positional correction quantity  $dX(t)$  is calculated from these and the encoder output pulse cycle  $T(t)$  from the timer (31) using equation (3).

The adder (33) adds a value 16 times the first position information CNT1, the second position information CNT2, and the positional correction quantity  $dX(t)$  to obtain a corrected position  $X_i(t)$ . The sum CNT ( $= CNT1 \times 16 + CNT2$ ) of 16 times the first position information CNT1 and the second position information CNT2 represents the current position  $X(t)$  of the carriage (15) at a resolution of 2400 dpi. Therefore, the corrected position  $X_i(t)$ , or the sum of the current position  $X(t)$  and the positional correction quantity  $dX(t)$ , represents a dot position on the image which is hit by ink ejected at the current carriage position  $X(t)$ .

The X motor control section (28) receives the first position information CNT1 and the encoder output pulse cycle T(t). Based on these inputs, the X motor control section (28) controls the X motor (21) to control the movement of the carriage (15).

The head control section (28) receives the corrected position  $X_i(t)$  and the dot position  $X_d$  on the image from the adder (33). When the corrected position  $X_i(t)$  matches the dot position  $X_d$  on the image, the head control section (26) ejects ink in a manner corresponding to the dot position  $X_d$ .

The encoder (22) and the first U/D counter (29) form position sensing means for the carriage (15). The encoder (22), the first U/D counter (29), and the timer (31) form speed sensing means for the carriage (15). The first U/D counter (29) forms approximate position sensing means for the carriage (15). The second U/D counter (30) and the interval timer (32) form position details sensing means for the carriage (15). The timer (31) forms time measurement means. The TBL memory (33) forms correction quantity determining means. The head control section (26) forms ejection control means.

Next, referring to flow charts in Figure 11 to Figure 14 will an example of processes be described.

Figure 11 shows an example of a count process of the first position information by the first U/D counter (29).

In Figure 11, as the first U/D counter (29) is activated, first, an edge is examined as to whether it is a rising edge of the signal A (S1). If not, it is examined as to whether it is a falling edge of the signal A (S2). If not, the process returns to S1. If it is a rising edge of the signal A in S1, it is examined as to whether the signal B is L (low level) (S3). If not, the process returns to S1. If the signal B is L in S3, 1 is added to the first position information CNT1 (S4).

In contrast, if it is a falling edge of the signal A in S2, it is examined whether the signal B is L (S5). If not, the process returns to S1. If the signal B is L in S5, 1 is subtracted from the first position information CNT1 (S6).

After the completion of S4 or S6, an interrupt process is executed by the first U/D counter (29) in the timer (31) (detailed later) (S7). Then, it is examined as to whether the counter has stopped (S8). If not, the process returns to S1. If so, the process ends.

In a forward movement, as would be obvious from Figure 10, the signal B is H (high level) at a falling edge of the signal A. Therefore, even if the process goes from S1 and S2 to S5, it does not return to S1 and continue at S6. In addition, at a rising edge of the signal A, the signal B is L. Therefore, when the process goes from S1 to S3, it goes on to S4 where 1 is added to the first position information CNT1. Then, every time a rising edge of the signal A is sensed, the first position

information CNT1 is incremented by 1. This corresponds to the carriage (15) moving toward the positive side of the x axis in the forward movement.

In a return movement, as would be obvious from Figure 10, the signal B is H (high level) at a rising edge of signal A. Therefore, even if the process goes from S1 to S3, it does not return to S1 and continue at S4. In addition, at a falling edge of the signal A, the signal B is L. Therefore, when the process goes from S1 and S2 to S5, it goes on to S6 where 1 is subtracted to the first position information CNT1. Then, every time a falling edge of the signal A is sensed, the first position information CNT1 is decremented by 1. This corresponds to the carriage (15) moving toward the negative side of the x axis in the return movement.

Figure 12 shows an example of the interrupt process in S7 in Figure 11.

In Figure 12, first, the time-measure count (timer value)  $T_n$  of the timer (31) is read (S71), and the last time measurement reading  $T_{n-1}$  is retrieved from a built-in timer value memory (S72). Then, from these, a latest pulse cycle  $T(t)$  ( $= T_n - T_{n-1}$ ) is calculated (S73) which is output to the TBL memory (33) (S74). Next, the count of the pulse cycle  $T(t)$  is right-shifted by 4 bits to divide it by 16 (S75). The interval timer (32) is set to the result (S76), and the interval timer (32) is activated (S77).



Then, it is determined whether the carriage (15) is in a forward movement (S78). If so, the second position information CNT2 is set to 0 (S79). If not, the second position information CNT2 is set to 15 (S80). After the completion of S79 or S80, the reading of the time-measure count  $T_n$  obtained in S71 is written to a timer value memory (S81) before the process ends.

Figure 13 shows an example of the interrupt process by the interval timer (32) in the second U/D counter (30). The process is executed every time the interval timer (32) outputs a timeout signal TMOU.

In Figure 13, first, it is determined whether the carriage (15) is in a forward movement (S11). If so, 1 is added to the second position information CNT2 (S12). Thereafter, it is determined whether the second position information CNT2 is 15 (S13). If not, the process ends. If the second position information CNT2 is 15 in S13, the interval timer (32) is stopped (S14) before the process ends.

In contrast, if the carriage (15) is in a return movement in S11, 1 is subtracted from the second position information CNT2 (S15). Thereafter, it is determined whether the second position information CNT2 is 0 (S16). If not, the process ends. If the second position information CNT2 is 0 in S16, the interval timer (32) is stopped (S17) before the process ends.

In a forward movement, the second position information

CNT2 is set to 0 in S79 in the flow chart in Figure 12. For this reason, until the flow chart in Figure 12 is executed next time, in other words, until a next rising edge of the signal A, S12 in the flow chart in Figure 13 is executed 15 times to increment the second position information CNT2 from 0 to 15 by 1.

In a return movement, the second position information CNT2 is set to 15 in S80 in the flow chart in Figure 12. For this reason, until the flow chart in Figure 12 is executed next time, in other words, until a next falling edge of the signal A, S15 in the flow chart in Figure 13 is executed 15 times to decrement the second position information CNT2 from 15 to 0 by 1.

Therefore, both in the forward movement and in the return movement, the 2400 dpi position information of the carriage (15) is obtained by adding the first position information CNT1 multiplied by 16 to the second position information CNT2.

Figure 14 shows an example of a process by the adder (34) and another process by the head control section (26).

In Figure 14, first, the positional correction quantity  $dX(t)$  is retrieved from the TBL memory (33) (S21). The current position  $X(t)$  of the carriage (15) is computed as given by equation (9) (S22).

$$X(t) = CNT1 \times 16 + CNT2 \dots (9)$$

Next, a corrected position computing step (S23) is executed. In other words, first, it is determined whether the carriage (15) is in a forward movement (S231). If so, the positional correction quantity  $dX(t)$  is added to the current position  $X(t)$  to obtain the corrected position  $X_i(t)$  (S232). If it is determined in S231 that the carriage (15) is in a return movement (S231), the positional correction quantity  $dX(t)$  is subtracted from the current position  $X(t)$  to obtain the corrected position  $X_i(t)$  (S233).

After the completion of the corrected position computing step in S23, it is determined whether the corrected position  $X_i(t)$  matches the dot position  $X_d$  on the image (S24). If not, the process returns to S21. If the corrected position  $X_i(t)$  match the dot position  $X_d$  in S24, ink is ejected corresponding to the dot position  $X_d$  (S25). Then, it is determined whether ink ejection (print) for the print area is complete (S26). If not, the process returns to S21. If so, the process ends.

When the ink ejection control is done based on the double-direction positional correction quantity obtained from the encoder output pulse cycle, the TBL memory (33) holds the reference encoder output pulse cycle  $T_0$  and the double-direction reference positional correction quantity  $dX_1$  when the carriage (15) is moving a the reference speed  $V_0$ . From these and the encoder output pulse cycle  $T(t)$  from the

timer (31), the positional correction quantity  $dX(t)$  can be given by equation (4). In addition, in the flow chart in Figure 14, the corrected position computing step of S23 is replaced by the step in Figure 15.

5           In Figure 15, first, it is determined whether the carriage (15) is moving in a forward movement (S234). If so, the current position  $X(t)$  is set to the corrected position  $X_i(t)$  (S235). In S234, if it is determined that the carriage (15) is moving in a return movement, the positional correction  
10           quantity  $dX(t)$  is subtracted from the current position  $X(t)$  to obtain the corrected position  $X_i(t)$  (S236).

Otherwise, the same ink ejection control based on the single-direction positional correction quantity is implemented.

15           In the example, to represent the position of the carriage (15), position information is applied to the two sets of information, i.e. the first position information CNT1 (150 dpi) and the second position information CNT2 (2400 dpi).

A single set of position information made up of the first position information and the second position information  
20           appended as lower order digits to the first position information can represent the position of the carriage (15).

Figure 16 shows functions and arrangement the control section (24) which is a part related to the ink ejection control under these conditions. As shown in the figure, the control  
25           section (24) includes a U/D counter (35), a timer (36), an

interval timer (37), a TBL memory (38), and an adder (39).

The timer (36) and the TBL memory (38) are arranged similarly to the timer (31) and the TBL memory (33) in Figure 9. In addition, the interval timer (37) operates similarly to the interval timer (32) in Figure 9, but differs from it where the timeout signal TMOU, or an output signal, is fed to the U/D counter (35).

The U/D counter (35) is a 16 bit counter. The counter (35) counts the output pulses from the encoder (22) using the higher order 12 bits (first position information) and timeout signals TMOU from the interval timer (37) using the lower order 4 bits (second position information), so as to obtain 2400 dpi position information CNT. The position information CNT represents nothing but the current position  $X(t)$  of the carriage (15).

The adder (39) determines a corrected position  $X_i(t)$  by adding the position information CNT which represents the current position  $X(t)$  of the carriage (15) and the positional correction quantity  $dX(t)$  obtained by the TBL memory (38).

The X motor control section (28) receives the higher order 12 bits of the position information CNT and the encoder output pulse cycle  $T(t)$ . On the basis of these, the X motor control section (28) controls the X motor (21) to controls the movement of the carriage (15).

The encoder (22) and the U/D counter (35) form the

position sensing means for the carriage (15). The encoder (22),  
the U/D counter (35), and the timer (36) form the speed  
sensing means for the carriage (15). The U/D counter (35)  
forms the approximate position sensing means for the  
5 carriage (15). The U/D counter (35) and the interval timer (37)  
form the position details sensing means for the carriage (15).  
The timer (36) forms the time measurement means. The TBL  
memory (38) forms the correction quantity determining means.  
The head control section (26) forms the ejection control  
10 means.

Figure 17 shows an example of a count process by the  
U/D counter (35) using the higher order 12 bits.

In Figure 17, as the U/D counter (35) is activated, first,  
an edge is examined whether it is a rising edge of the signal A  
15 (S31). If not, it is examined whether it is a falling edge of the  
signal A (S32). If not, the process returns to S31. If it is a  
rising edge of the signal A in S31, it is examined whether the  
signal B is L (low level) (S33). If not, the process returns to  
S31. If the signal B is L in S33, the position information CNT  
20 is set to the AND (AND) of the position information CNT at  
that time and [FFF0] (S34), and the [10] is added to the  
position information CNT (S35).

In contrast, if it is a falling edge of the signal A in S32,  
it is examined whether the signal B is L (S36). If not, the  
25 process returns to S31. If the signal B is L in S36, the

position information CNT is set to the AND of the position information CNT and [FFF0] (S37), [10] is subtracted from the position information CNT (S38), and [F] is added to the position information CNT (S39).

5           After the completion of S35 or S39, an interrupt process by the U/D counter (35) in the timer (36) is implemented (S40). This is the same interrupt process as the one in S7 in the flow chart in Figure 11. Then, it is examined whether the counter has stopped (S40). If not, the process returns to S31.  
10       If so, the process ends.

          In a forward movement, as explained earlier, every time a rising edge of the signal A from the encoder (22) is sensed, the higher order 12 bits of the position information CNT is incremented by 1. In addition, when the process in the flow  
15       chart in Figure 17 ends, the lower order 4 bits of the position information CNT is 0. Every time a timeout signal TMOUT is fed from the interval timer (37), the lower order 4 bits of the position information CNT is incremented by 1. Since the  
20       timeout signal TMOUT is fed 15 times before a next rising edge of the signal A is sensed, the lower order 4 bits of the position information CNT is incremented from 1 to 15. As a result, the entire position information CNT is incremented by  
25       1 on each input of a timeout signal TMOUT. This corresponds to the carriage (15) moving toward the positive side of the x axis in the forward movement.

In a return movement, as explained earlier, every time a falling edge of the signal A from the encoder (22) is sensed, the higher order 12 bits of the position information CNT is decremented by 1. In addition, when the process in the flow chart in Figure 17 ends, the lower order 4 bits of the position information CNT is 15. Every time a timeout signal TMOUT from the interval timer (37) is fed, the lower order 4 bits of the position information CNT is decremented by 1. Since the timeout signal TMOUT is fed 15 times before a next falling edge of the signal A is sensed, the lower order 4 bits of the position information CNT is decremented from 15 to 0. As a result, the entire position information CNT is decremented by 1 on each input of a timeout signal TMOUT. This corresponds to the carriage (15) moving toward the negative side of the x axis in the return movement.

In the embodiment, the present invention has been applied to inkjet printers which prints on paper. Alternatively, the present invention is applicable to any given device utilizing inkjet technology, including manufacturing steps for color filters in liquid crystal panels, organic EL panels, light switch elements, printed wiring boards, and electronic circuits.

In addition, the members and process steps related to the control section (24) in the inkjet print device of the embodiment can be realized by a CPU or other compute means



executing computer programs contained in a ROM, RAM, or other storage means to control periphery devices. Therefore, a computer equipped with these means can realize various functions and processes related to the control section (24) in the inkjet print device of the present embodiment merely by reading a storage medium containing the computer program and executing the computer program. In addition, if the computer program is contained in a removable storage medium, the various functions and processes can be realized on any given computer.

Such a computer program storage medium may be a memory (not shown), such as a ROM, so that the process is executable on a microcomputer. Alternatively, a program medium may be used which can be read by inserting the storage medium in an external storage device (program reader device; not shown).

In addition, in either of the cases, it is preferable if the contained program is accessible to a microprocessor which will execute the program. Further, it is preferable if the program is read, and the program is then downloaded to a program storage area of a microcomputer where the program is executed. Assume that the program for download is stored in a main body device in advance.

In addition, the program medium is a storage medium arranged so that it can be separated from the main body.

Examples of such a program medium include a tape, such as a magnetic tape and a cassette tape; a magnetic disk, such as a flexible disk and a hard disk; a disc, such as a CD/MO/MD/DVD; a card, such as an IC card (inclusive of a memory card); and a semiconductor memory, such as a mask ROM, an EPROM (erasable programmable read only memory), an EEPROM (electrically erasable programmable read only memory), or a flash ROM. All these storage media hold a program in a fixed manner.

Alternatively, if a system can be constructed which can connects to the Internet or other communications network, it is preferable if the program medium is a storage medium carrying the program in a flowing manner as in the downloading of a program over the communications network.

Further, when the program is downloaded over a communications network in this manner, it is preferable if the program for download is stored in a main body device in advance or installed from another storage medium.

As in the foregoing, an inkjet print device in accordance with the present invention is arranged to include: position sensing means for sensing the carriage position; speed sensing means for sensing moving speed of the carriage; correction quantity determining means for presetting a relationship between the carriage speed and a positional correction quantity for correcting a discrepancy in an ink

hitting position resulting from the ink ejection from the print head while the carriage is moving and for determining the positional correction quantity from the carriage speed sensed by the speed sensing means according to the preset relationship; and ejection control means for controlling the ink ejection from the print head according to the positional correction quantity determined by the correction quantity determining means and the carriage position sensed by the position sensing means.

It is desirable if the correction quantity determining means is activated at least when the carriage is either accelerating or decelerating.

Thus, even if the carriage speed changes, the ink ejection from the print head is controlled with a suitable positional correction quantity. Thus, good image quality is available even while the carriage is accelerating or decelerating. Hence, the device can print in the accelerate/decelerate areas flanking the constant-speed area, achieving reduced print time and reduced device size.

The positional correction quantity may be a difference of the ink hitting position from a position of the ink ejection from the print head. When this is the case, the positional correction quantity substantially proportional to the carriage speed. Therefore, simple proportionality computation can achieve a suitable positional correction quantity (detailed

later).

In addition, the positional correction quantity may be a difference between an ink hitting position in the forward movement and an ink hitting position in the return movement related to a certain ink eject position of the print head. When this is the case, the positional correction quantity is substantially proportional to the carriage speed. Therefore, simple proportionality computation can achieve a suitable positional correction quantity (detailed later).

Further, when this is the case, the ejection control means controls ink ejection with the positional correction quantity being 0 in either one of the forward movement and the return movement. In other words, the ink eject position does not need to be corrected in either one of the forward movement and the return movement.

Another inkjet print device in accordance with the present invention is arranged as in the foregoing, and characterized in that the relationship between the carriage speed and the positional correction quantity is a proportional relationship.

According to the arrangement, a certain carriage speed is designated as a reference carriage speed, and a positional correction quantity at the reference carriage speed is designated as a reference positional correction quantity. With the reference carriage speed and the reference positional

correction quantity being prestored, proportionality computation can determine the positional correction quantity from the carriage speed sensed by the speed sensing means. Therefore, simple proportionality computation can achieve a  
5 suitable positional correction quantity.

Another inkjet print device in accordance with the present invention is arranged as in the foregoing, and characterized in that the correction quantity determining means prestores a certain carriage speed and a positional  
10 correction quantity at that carriage speed as a respective reference carriage speed  $V_0$  and also prestores a reference positional correction quantity  $dX_0$  and determines the positional correction quantity  $dX(t)$  from the moving speed  $V(t)$  of the carriage sensed by the speed sensing means as  
15 given by equation (1):

$$dX(t) = dX_0 \times V(t)/V_0 \dots (1)$$

For example, the difference of the ink hitting position from an ink eject position of the print head is designated as a positional correction quantity. An ink eject position at a  
20 reference carriage speed  $V_0$  is  $X_h$ . An ink hitting position is  $X_p$ . The reference positional correction quantity  $dX_0$  is then given by equation (5):

$$dX_0 = X_p - X_h \dots (5)$$

In addition, the ink eject position at a carriage speed  
25  $V(t)$  sensed by the speed sensing means is  $X_h(t)$ . An ink

hitting position is  $X_p(t)$ . The positional correction quantity  $dX(t)$  is then given by equation (6):

$$dX(t) = X_p(t) - X_h(t) \dots (6)$$

As explained earlier, the positional correction quantity  $dX(t)$  at a given carriage speed  $V(t)$  is substantially proportional to the carriage speed  $V(t)$ . Therefore, the positional correction quantity  $dX(t)$  is given by equation (1). Thus, the positional correction quantity can be determined by a simple equation.

When the difference of the ink hitting position from an ink eject position of the print head is a positional correction quantity, ink ejection is controlled according to the positional correction quantity determined as above both in the forward movement and in the return movement.

In addition, for example, a difference between an ink hitting position in the forward movement and an ink hitting position in the return movement related to a certain ink eject position of the print head is a positional correction quantity. An ink eject position at the reference carriage speed  $V_0$  is  $X_h$ . An ink hitting position in the forward movement is  $X_f$ . An ink hitting position in the return movement is  $X_r$ . The reference positional correction quantity  $dX_1$  is then given by equation (7):

$$dX_1 = X_f - X_r \dots (7)$$

In addition, an ink eject position at the carriage speed

V(t) sensed by the speed sensing means is  $X_h(t)$ . An ink hitting position in the forward movement is  $X_f(t)$ . An ink hitting position in the return movement is  $X_r(t)$ . The positional correction quantity  $dX(t)$  is given by equation (8):

5            $dX(t) = X_f(t) - X_r(t) \dots (8)$

          This is a sum of a difference of the ink hitting position  $X_f(t)$  in the forward movement from the ink eject position  $X_h(t)$  and a difference of the ink hitting position  $X_r(t)$  in the return movement from the ink eject position  $X_h(t)$ , and  
10           therefore is substantially proportional to the carriage speed  $V(t)$ . Therefore, the positional correction quantity  $dX(t)$  can be determined by substituting  $dX_1$  for  $dX_0$  in equation (1). Thus, the positional correction quantity can be determined by a simple equation.

15           When the difference between the ink hitting position in the forward movement and the ink hitting position in the return movement related to the certain ink eject position of the print head is a positional correction quantity, the positional correction quantity is rendered 0 and the ink eject  
20           position does no need to be corrected in either one of the forward movement and the return movement.

          Therefore, according to the arrangement, a suitable positional correction quantity can be achieved through simple equation (1).

25           Another inkjet print device in accordance with the

present invention is arranged as in the foregoing, and characterized in that the correction quantity determining means prestores a correction quantity table representing a relationship between multiple carriage speeds and multiple positional correction quantities and determines the positional correction quantity from the carriage speed sensed by the speed sensing means in reference to the correction quantity table.

The correction quantity table is created, for example, from a positional correction quantity at a certain carriage speed by proportionality computation.

According to the arrangement, a suitable positional correction quantity can be readily achieved using the correction quantity table.

Another inkjet print device in accordance with the present invention is arranged as in the foregoing, and characterized in that the position sensing means contains an encoder producing a pulse signal output according to a displacement of the carriage; the speed sensing means contains time measurement means for measuring a cycle of the pulse output from the encoder; and the correction quantity determining means presets a relationship between the output pulse cycle and the positional correction quantity and determines the positional correction quantity from the cycle of the pulse output measured by the time measurement



means according to the preset relationship.

Here, the time measurement means in the speed sensing means can sense the output pulse cycle of the encoder by, for example, counting predetermined clock pulses. When this is the case, the output pulse cycle can be obtained as a count by the time measurement means.

According to the arrangement, the time measurement means measures an output pulse cycle according to a pulse signal output from the encoder. The correction quantity determining means obtains a suitable positional correction quantity from the output pulse cycle measured by the time measurement means. Therefore, a suitable positional correction quantity can be quickly obtained according to signals from well known devices, such as the timer and the encoder which form the time measurement means. Thus, efficiency in the inkjet print process is improved.

Another inkjet print device in accordance with the present invention is arranged as in the foregoing, and characterized in that the relationship between the output pulse cycle and the positional correction quantity is an inversely proportional relationship.

The output pulse cycle of the encoder is inversely proportional to the carriage speed. Therefore, according to the arrangement, the output pulse cycle is inversely proportional to the positional correction quantity; therefore, similarly to

the case where the aforementioned carriage speed is proportional to the positional correction quantity, the certain output pulse cycle designated as is a reference output pulse cycle, and a positional correction quantity at the reference output pulse cycle as a reference positional correction quantity. With these reference output pulse cycle and reference positional correction quantity being prestored, inverse proportionality computation can provide a positional correction quantity from the output pulse cycle sensed by the encoder and the time measurement means. Therefore, simple calculation can determine a suitable positional correction quantity.

Another inkjet print device in accordance with the present invention is arranged as in the foregoing, and characterized in that the correction quantity determining means prestores the output pulse cycle  $T_0$  at a certain speed  $V_0$  of the carriage and the positional correction quantity  $dX_0$  and determines the positional correction quantity  $dX(t)$  from the output pulse cycle  $T(t)$  measured by the time measurement means in the speed sensing means as given by equation (3):

$$dX(t) = dX_0 \times T_0 / T(t) \dots (3)$$

As explained earlier, the positional correction quantity  $dX(t)$  at a given carriage speed  $V(t)$  is substantially inversely proportional to the output pulse cycle of the encoder  $T(t)$ .

Therefore, the positional correction quantity  $dX(t)$  is given by equation (3). Thus, a suitable positional correction quantity can be determined through simple equation (3).

Another inkjet print device in accordance with the present invention is arranged as in the foregoing, and characterized in that

the correction quantity determining means prestores a correction quantity table representing a relationship between the multiple output pulse cycles and multiple positional correction quantities and determines the positional correction quantity from the output pulse cycle measured by the time measurement means in the speed sensing means in reference to the correction quantity table.

The correction quantity table can be created, for example, through inverse proportionality computation on the positional correction quantity at a certain output pulse cycle.

According to the arrangement, a suitable positional correction quantity can be readily determined using the correction quantity table.

Another inkjet print device in accordance with the present invention is arranged as in the foregoing, and characterized in that the device further includes position details sensing means for dividing the output pulse cycle time-measured by the time measurement means and counting

every time the divided cycle elapses so as to sense position details of the carriage.

According to the arrangement, the output pulse cycle is divided, and every time the divided cycle elapses, counted. Therefore, carriage position details are determined at a higher resolution than the encoder resolution. Controlling the ink ejection according to the position details can achieve high resolution printing.

Assuming, for example, that the encoder resolution is 150 dpi, and the output pulse cycle is divided by 16, the resolution of the carriage position details is 2400 ( $= 150 \times 16$ ) dpi.

Another inkjet print device in accordance with the present invention is arranged as in the foregoing, and characterized in that the time measurement means obtains the output pulse cycle as digital data; and the position details sensing means shifts data of the output pulse cycle time-measured by the time measurement means toward the right by a predetermined number of times so as to divide the output pulse cycle.

According to the arrangement, the output pulse cycle can be readily divided merely by shifting the data of the output pulse cycle time-measured by the time measurement means. Thus, the carriage position details can be readily determined.

When this is the case, the number by which the cycle is divided is a power of 2. Its power indicates the number of shifts.

5 Another inkjet print device in accordance with the present invention is arranged as in the foregoing, and characterized in that the position sensing means contains approximate count means for measuring a number of pulses of the pulse signal output from the encoder; and a combined value of a count by the approximate coefficient means as high  
10 order digits and a count by the details count means as low order digits is the carriage position.

The position details sensing means may determine an absolute position of the carriage or a relative position of the carriage. To determine a relative position of the carriage, the  
15 position sensing means further contains approximate position sensing means which senses an approximate position of the carriage by measuring the number of pulses of the pulse signal output from the encoder. With the count by the approximate position sensing means being designated as high  
20 order digits, the count by the position details sensing means as low order digits, and the combined value as the carriage position, the absolute position of the carriage can be determined.

A method of controlling an inkjet print device in  
25 accordance with the present invention a method of controlling

an inkjet print device which prints by reciprocally moving a carriage carrying a print head in a main scan direction while controlling ink ejection from the print head according to a carriage position both in a forward movement and in a return movement, the device including position sensing means for sensing the carriage position and speed sensing means for sensing moving speed of the carriage, the method including: the relationship setting step of presetting a relationship between the moving speed of the carriage and a positional correction quantity for correcting a discrepancy in an ink hitting position resulting from the ink ejection from the print head while the carriage is moving; the correction quantity determining step of determining the positional correction quantity from the moving speed of the carriage sensed by the speed sensing means according to the relationship preset in the relationship setting step; the ejection control step of controlling the ink ejection from the print head according to the positional correction quantity determined in the correction quantity determining step and the carriage position sensed by the position sensing means.

According to the method, even if the carriage speed changes, a suitable positional correction quantity can be determined according to the relationship between the positional correction quantity and the carriage speed. Thus, the ink ejection from the print head is controlled with the

suitable positional correction quantity. Good image quality is available even while the carriage is accelerating or decelerating. Hence, the device can print in the accelerate/decelerate areas flanking the constant-speed area, achieving reduced print time and reduced device size.

The correction quantity determining means and the ejection control means in the inkjet print device can be realized by an inkjet print program on a computer. Further, by storing the inkjet print program on a computer-readable storage medium, the inkjet print program can be executed on any given computer.

The embodiments and examples described in *Best Mode for Carrying Out the Invention* are for illustrative purposes only and by no means limit the scope of the present invention. Variations are not to be regarded as a departure from the spirit and scope of the invention, and all such modifications as would be obvious to one skilled in the art are intended to be included within the scope of the claims below.

## INDUSTRIAL APPLICABILITY

According to the present invention, an inkjet print device is provided capable of determining a suitable positional correction quantity even if the moving speed of the carriage changes and achieving good image quality even while the device is accelerating or decelerating.

Thus, the device can print in the accelerate/decelerate areas flanking the constant-speed area, achieving reduced print time and reduced device size.